

RESEARCH ON ABRASIVENESS OF MATERIALS USED ON FINISHING METAL ALLOYS. PART I

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Abstract: *In magneto-abrasive processes, the working environment consists of magneto-abrasive powder (ferromagnetic particles such as ferrite or composite powders) or from suspensions, namely ferrofluids or magneto-rheological liquids. Abrasive materials are natural or synthetic crystalline substances with high hardness, used for grinding or polishing materials. To achieve the required materials for finishing metal alloys, metal waste (steel and iron chips) granite, grinding wheels and siliceous sand waste were used. This article aims to present the logistics used to obtain the materials, study the abrasiveness of different materials and their combinations, and to determine the final roughness of the samples used.*

Keywords: *abrasiveness, roughness, abrasive materials*

1. General Introduction

The general feature, common to abrasive processes, is the use of abrasives (powders or granules) arranged in a given carrying environment. It may be possible to make different abrasive environments, which, depending on the way they are constituted, make the difference between the technological processes. [7]

Abrasive grains can be placed in a binder and compacted in abrasive bodies with well-defined forms, used in regrinding operations. This way, an abrasive environment is created, having wide spread use.

Abrasive materials are presented in form of very tough granules, with sharp edges and tips, which disengage very small chips from working areas [7].

In order to detach the chips, the abrasive grains are driven in a relative movement against the work piece, being embedded in a solid object (abrasive discs), in a liquid (suspensions, paste), in a steam shot or in a magnetic field.

In order to establish the maximum performance of these working environments and to improve the quality of the surfaces a collaboration between metallurgists and technologists is needed [1].

2. The equipment used in manufacturing and determining materials abrasiveness and roughness

2.1 Equipment used for obtaining metal powder [2], [3], [4]

In order to obtain metal powder used in magneto-abrasive materials, a ball mill has been designed (figure 1). The equipment is designed and constructed to prepare metal waste (chips etc.), in order to re-use it for finishing magneto-abrasive operations or with other purposes.

The equipment is made of a metal case (7), in which there are steel balls (17). The equipment is driven by an engine (14), which transmits rotary motion to the mill case (7) with the aid of the belt pulley (11,15) through a drive belt (13).

Through mill rotating, the balls (17) keep the same direction as the rotating movement. This movement takes place as long as the tilt angle of the load, at a given moment, stays lower than the normal slope angle on which the rolling or falling of the grinding material take place. This way, through friction and collision, the

fragmentation of the material subjected to grinding takes place.

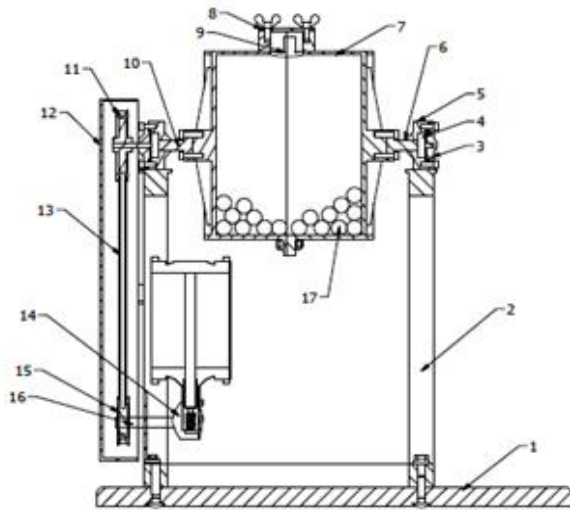


Figure 1: Equipment for grinding metal waste (Ball mill); scheme of the ball mill: 1 – Mill bed, 2 – Frame, 3 - Bearing cover, 4 – Bearing, 5 - Bearing Support, 6-10 - Drive shafts, 7 – Mill case, 8 - Cover, 9 – Admission hopper, 11-15 – Belt pulley, 12 – Case, 13 -Drive Belt, 14 – Motor, 16 - Motor shaft, 17 – Balls

The following factors act on the intensity and mechanism of the fragmentation process (Co, '97)):

- the rotation speed of the mill;
- the ratio of the diameter (D) and the length (L) of the mill case (D/L);
- the weight and diameter of the grinding material;
- the volume of material subjected to grinding;
- grinding time;
- the environment in which the grinding process takes place.

The metal waste (steel chips, iron cast) used to obtain metal powders, were taken from those resulted after cutting processes like turning, milling, drilling, grinding, broaching etc.), from various companies and from the cutting tools laboratory of the Faculty of Mechanical Engineering, Mechatronics and Management.

For a charging of $m=0,750$ kg of waste, 0,232 kg of metal powder was obtained in a period of time $t=6$ hours, using a number of 60 balls with a diameter of $\varnothing 20$ mm. The mill is powered with a direct current (D.C.) motor of 24 V and an amperage of 5A.

The powder obtained was subjected to a sieving procedure using an equipment with mechanical sieving through horizontal and vertical vibration type PSS, in a time period $t=15$ minutes. The electromagnetic sieving device for sieves with a diameter of 200 mm, (in accordance with EN 932-5), located in the Laboratory of materials technology, it is powered by electromagnetic pulse and, because of its vibrating actions (vertical, lateral and rotating), it offers a high precision of results.

After the sieving process, metal powders, with different sizes were obtained, these being used for magneto-abrasive finishing, in combination with abrasive powder.

2.2 Equipment for studying material abrasiveness [5], [6]

For the abrasive part of the magneto-abrasive materials used for superfinishing the metal parts, the use and re-use of abrasive material waste (granite, siliceous sand and electrocorundum) from different companies was chosen. Thus, granite waste were purchased from Suceava, Radauti and the siliceous sand was purchased from Dorohoi. The waste of abrasive disks (electrocorundum) was obtained from various commercial

companies from Suceava area. The abrasive waste was separated from the iron filings (the grindings) with the help of magnets. In the same manner like metal powders, the electrocorundum was sieved using the equipment described above.

In order to study the abrasiveness of granite, siliceous sand and electrocorundum powder and the mixtures of these, a device has been designed as shown in figure 2.

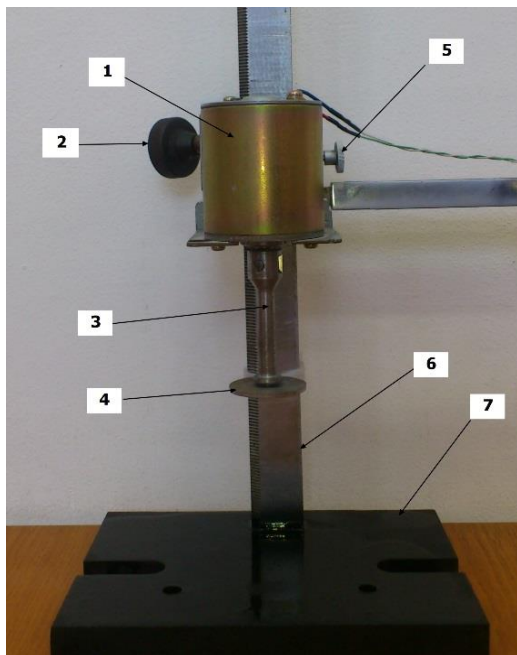


Figure 3 – Abrading device 1. D.C. motor (12V, 1A); 2. Motor handle; 3. Threaded rod (M6); 4. Sample; 5. Locking screw; 6. Support column; 7. Base plate

It is formed by a DC motor of 12V (1), on which rod the sample is screwed (4). The motor can be repositioned on the rod (6) in order to set the container with the powder and for immersion the sample (4) in the abrasive powder.

The samples on which the experiments were carried out, have been made of steel (OLC 45), a bar with a diameter of 45 mm (Figure 3).

For creating the samples, a normal lathe SN 320, from the multidisciplinary laboratory of the Faculty of Mechanical engineering, Mechatronics and Management was used. The cutting parameters used were as following: speed $n = 500$ rpm, feed $s = 0.18$ mm/rev, cutting depth $t = 3$ mm. The number of

multypass is 7, the thread M6x1 was made on a lathe, using a die head.

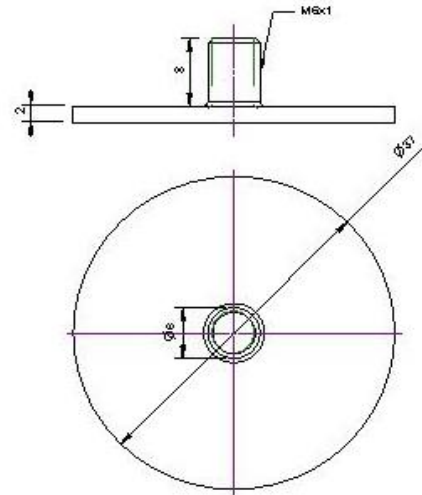


Figure 3: Sample's scheme

In order to study the roughness of the samples, two devices from the Faculty of Mechanical engineering, Mechatronics and Management were used: an optical scanning profilometer NANOFOCUS μ SCAN LASER PROFILOMETER (figure 4) and the Mahr Perthometer S2 type [9], [10], [11].



Figure 4 – a) Nanofocus μ Scan Laser Profilometer; b) Mahr Perthometer S2 type

In order to determinate the speed of the ball mill and the abrading device, a SHIMPO DT-209X-S12 tachometer, located in Mechanical and Technologies Department from the "Stefan cel Mare" University of Suceava was used.

3. Characterizing the materials' abrasiveness. Gathering the results and obtaining the mathematical model [5], [8]

The research carried out and presented here mainly aim to determinate the extent of influence of each technological parameter on

the level of final results characteristic (weight of material removed). Secondly, a determination of a mathematical correlation between the influences manifested by these parameters was aimed in such a way as to create a real possibility of control and rapid intervention in the process at the time when the one of parameters cannot be maintained at a preset value.

Taking into consideration that certain practical values (minimum value) of answers are followed, it is appropriate to establish interdependencies able to describe both the nature and the extent of the considered influences, therefore a mathematical model should be determined.

Hence the scientific literature consulted does not provide a proper mathematical solution, precise and operative in describing the interdependencies mentioned above, a mathematical model based on statistics was elaborated.

The mathematical models thus obtained will be subjected then to optimization.

In order to obtain the mathematical model a polynomial model with many variables was used:

– *independent variables*: speed (A), grain size (B), the exposure time (C);

– *dependent variable*: the quantity of removed material for each of the three materials (granite, siliceous sand and electrocorundum) and combinations between them (granite and siliceous sand, granite+electrocorundum, siliceous sand+electrocorundum, granite + siliceous sand + electrocorundum).

In order to present in a simple manner the experiments conducted, coded variables will be used for the levels of independent variables (factors). Thus, the following notations are done:

- 1 – the minimum level of a variable;
- 0 – the central level of a variable;
- +1 – the maximum level of a variable.

The system’s responses m_i (the weight of removed material) were also coded, using the following notations: $i = 1 \dots 63$, i being the number of experiment from the matrix of experiments.

Table 1 shows the codes for independent variables, as well as the correspondence between the real values and the coded ones taken into account for establishing the model.

To create the mathematical model, the program Design Expert was used.

Table 1: Symbolizing and correspondence between coded values and real values of independent variables

Variables	Symbols	The coded variables of real variables		
		-1	0	1
Speed [rpm]	A	700	850	1000
Grain size [mm]	B	0.04	0.17	0.3
Time [min]	C	30	60	90

3.2. Characterizing the granite abrasiveness [6]

Statistical Summary found mathematical models to describe the dependent variables is presented in Table 2.

Table 2. Statistical summary of proposed mathematical models

Dependent variable	Model	Standard deviation [σ]	Regression coefficient [R^2]	Adjusted regression coefficient [R^2 adjusted]
m_1	2 nd order polynomial	0,0011050	0,9640	0,9573
m_2	2 nd order polynomial	0,0007566	0,9680	0,9598
m_3	2 nd order polynomial	0,0028440	0,9710	0,9605
m_4	2 nd order polynomial	0,0010190	0,9750	0,9585
m_5	2 nd order polynomial	0,0018400	0,9710	0,9662
m_6	2 nd order polynomial	0,0021300	0,9550	0,9522
m_7	2 nd order polynomial	0,0015490	0,9610	0,9515

Table 7. Experimental data for mixture of granite and electrocorundum

Mixture of granite and electrocorundum									
No.	Speed [rpm]	Grain size [mm]	Time [min]	Removed material [g]	No.	Speed [rpm]	Grain size [mm]	Time [min]	Removed material [g]
1	700	0.063	30	0.0020	32	850	0.1	60	0.0085
2	700	0.05	30	0.0017	33	850	0.15	60	0.0113
3	700	0.04	30	0.0010	34	850	0.2	60	0.0110
4	700	0.1	30	0.0033	35	850	0.3	60	0.0153
5	700	0.15	30	0.0053	36	1000	0.063	60	0.0042
6	700	0.2	30	0.0055	37	1000	0.05	60	0.0039
7	700	0.3	30	0.0062	38	1000	0.04	60	0.0032
8	850	0.063	30	0.0024	39	1000	0.1	60	0.0095
9	850	0.05	30	0.0016	40	1000	0.15	60	0.0123
10	850	0.04	30	0.0011	41	1000	0.2	60	0.0113
11	850	0.1	30	0.0046	42	1000	0.3	60	0.0192
12	850	0.15	30	0.0063	43	700	0.063	90	0.0051
13	850	0.2	30	0.0065	44	700	0.05	90	0.0046
14	850	0.3	30	0.0083	45	700	0.04	90	0.0029
15	1000	0.063	30	0.0023	46	700	0.1	90	0.0100
16	1000	0.05	30	0.0018	47	700	0.15	90	0.0134
17	1000	0.04	30	0.0014	48	700	0.2	90	0.0183
18	1000	0.1	30	0.0049	49	700	0.3	90	0.0179
19	1000	0.15	30	0.0061	50	850	0.063	90	0.0076
20	1000	0.2	30	0.0073	51	850	0.05	90	0.0060
21	1000	0.3	30	0.0106	52	850	0.04	90	0.0041
22	700	0.063	60	0.0030	53	850	0.1	90	0.0148
23	700	0.05	60	0.0025	54	850	0.15	90	0.0226
24	700	0.04	60	0.0016	55	850	0.2	90	0.0193
25	700	0.1	60	0.0067	56	850	0.3	90	0.0259
26	700	0.15	60	0.0091	57	1000	0.063	90	0.0082
27	700	0.2	60	0.0086	58	1000	0.05	90	0.0066
28	700	0.3	60	0.0109	59	1000	0.04	90	0.0050
29	850	0.063	60	0.0037	60	1000	0.1	90	0.0166
30	850	0.05	60	0.0033	61	1000	0.15	90	0.0198
31	850	0.04	60	0.0020	62	1000	0.2	90	0.0228
					63	1000	0.3	90	0.0323

Table 8. Experimental data for mixture of granite and siliceous sand

Mixture of granite and siliceous sand									
No.	Speed [rpm]	Grain size [mm]	Time [min]	Removed material [g]	No.	Speed [rpm]	Grain size [mm]	Time [min]	Removed material [g]
1	700	0.063	30	0.0012	32	850	0.1	60	0.0053
2	700	0.05	30	0.0009	33	850	0.15	60	0.0076
3	700	0.04	30	0.0006	34	850	0.2	60	0.0072
4	700	0.1	30	0.0018	35	850	0.3	60	0.0101
5	700	0.15	30	0.0033	36	1000	0.063	60	0.0025
6	700	0.2	30	0.0033	37	1000	0.05	60	0.0022
7	700	0.3	30	0.0038	38	1000	0.04	60	0.0022
8	850	0.063	30	0.0013	39	1000	0.1	60	0.0061
9	850	0.05	30	0.0008	40	1000	0.15	60	0.0082
10	850	0.04	30	0.0005	41	1000	0.2	60	0.0074
11	850	0.1	30	0.0028	42	1000	0.3	60	0.0132
12	850	0.15	30	0.0040	43	700	0.063	90	0.0033
13	850	0.2	30	0.0040	44	700	0.05	90	0.0026
14	850	0.3	30	0.0053	45	700	0.04	90	0.0017
15	1000	0.063	30	0.0011	46	700	0.1	90	0.0064
16	1000	0.05	30	0.0009	47	700	0.15	90	0.0089
17	1000	0.04	30	0.0005	48	700	0.2	90	0.0122
18	1000	0.1	30	0.0029	49	700	0.3	90	0.0120
19	1000	0.15	30	0.0039	50	850	0.063	90	0.0050
20	1000	0.2	30	0.0048	51	850	0.05	90	0.0039
21	1000	0.3	30	0.0071	52	850	0.04	90	0.0023
22	700	0.063	60	0.0017	53	850	0.1	90	0.0097
23	700	0.05	60	0.0013	54	850	0.15	90	0.0153
24	700	0.04	60	0.0007	55	850	0.2	90	0.0130
25	700	0.1	60	0.0045	56	850	0.3	90	0.0175
26	700	0.15	60	0.0060	57	1000	0.063	90	0.0053
27	700	0.2	60	0.0055	58	1000	0.05	90	0.0040
28	700	0.3	60	0.0073	59	1000	0.04	90	0.0031
29	850	0.063	60	0.0023	60	1000	0.1	90	0.0108
30	850	0.05	60	0.0018	61	1000	0.15	90	0.0131
31	850	0.04	60	0.0010	62	1000	0.2	90	0.0154
					63	1000	0.3	90	0.0220

Table 9. Experimental data for mixture of granite, siliceous sand and electrocorundum

Mixture of granite, siliceous sand and electrocorundum									
No.	Speed [rpm]	Grain size [mm]	Time [min]	Removed material [g]	No.	Speed [rpm]	Grain size [mm]	Time [min]	Removed material [g]
1	700	0.063	30	0.0018	32	850	0.1	60	0.0086
2	700	0.05	30	0.0016	33	850	0.15	60	0.0127
3	700	0.04	30	0.0010	34	850	0.2	60	0.0115
4	700	0.1	30	0.0037	35	850	0.3	60	0.0180
5	700	0.15	30	0.0043	36	1000	0.063	60	0.0050
6	700	0.2	30	0.0054	37	1000	0.05	60	0.0038
7	700	0.3	30	0.0061	38	1000	0.04	60	0.0028
8	850	0.063	30	0.0023	39	1000	0.1	60	0.0103
9	850	0.05	30	0.0017	40	1000	0.15	60	0.0129
10	850	0.04	30	0.0012	41	1000	0.2	60	0.0137
11	850	0.1	30	0.0045	42	1000	0.3	60	0.0200
12	850	0.15	30	0.0063	43	700	0.063	90	0.0055
13	850	0.2	30	0.0073	44	700	0.05	90	0.0049
14	850	0.3	30	0.0101	45	700	0.04	90	0.0032
15	1000	0.063	30	0.0027	46	700	0.1	90	0.0119
16	1000	0.05	30	0.0018	47	700	0.15	90	0.0137
17	1000	0.04	30	0.0013	48	700	0.2	90	0.0165
18	1000	0.1	30	0.0052	49	700	0.3	90	0.0198
19	1000	0.15	30	0.0067	50	850	0.063	90	0.0080
20	1000	0.2	30	0.0075	51	850	0.05	90	0.0062
21	1000	0.3	30	0.0116	52	850	0.04	90	0.0043
22	700	0.063	60	0.0031	53	850	0.1	90	0.0165
23	700	0.05	60	0.0027	54	850	0.15	90	0.0235
24	700	0.04	60	0.0017	55	850	0.2	90	0.0213
25	700	0.1	60	0.0068	56	850	0.3	90	0.0294
26	700	0.15	60	0.0080	57	1000	0.063	90	0.0093
27	700	0.2	60	0.0093	58	1000	0.05	90	0.0069
28	700	0.3	60	0.0106	59	1000	0.04	90	0.0051
29	850	0.063	60	0.0044	60	1000	0.1	90	0.0188
30	850	0.05	60	0.0033	61	1000	0.15	90	0.0225
31	850	0.04	60	0.0023	62	1000	0.2	90	0.0244
					63	1000	0.3	90	0.0331

4. Conclusions

Following the analysis of the experimental data, it appears that the best material removal

was done when using powders of abrasive waste (electrocorundum) a maximum quantity of material removed $m = 0,0607$ grams was

registered, followed, in order, by a powder mixture of granite and electrocorundum ($m = 0.03312$ g), a mixture of granite, siliceous sand and electrocorundum ($m = 0.0323$ g), a mixture of siliceous sand and electrocorundum ($m = 0,0312$ grams), granite powder ($m = 0.0244$ g), granite and siliceous sand mixture ($m = 0.022005$ g) and siliceous sand ($m = 0.0168$ g). These values were obtained at maximum speed and grain size respectively at 1,000 rpm and a grain size of 0.4mm. In other words, the impact of speed is negligible for small grains.

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